CST STUDIO SUITE[™] 2006B Application Note

Antenna Simulation



Farfield Terminology Broadband Farfield Farfield Optimization Co & Cross Polarization Phase Center / Grasp Export Circular Polarized Antennas



1 ube / v1.0 / 09. Nov 2006



pre-installed examples in CST STUDIO SUITE 2006



C:\Program Files\CST STUDIO SUITE 2006\ Examples\CST MICROWAVE STUDIO\ Transient Analysis\Antennas



How to generate the Farfield Info

- define farfield monitor at one or more specified frequencies
- box surface fields (E+H) are recorded, from which in the postprocessing the farfield is calculated.





Horn_01.zip

Farfield Terminology Online Help



CST MICROWAVE STUDIO

Farfield Overview

In CST MWS the used reference for gain/directivity is an ideal spherical radiator (=isotropic antenna -> dBi), a λ /2-Dipole has a gain of 2.2dB(i).

Some Farfield Terms

Directivity: The directivity of an antenna is officially defined as "the ratio of the radiation intensity in a given direction from the antenna to the radiation intensity averaged over all directions". At this the radiation intensity is given by the total power radiated by the antenna divided by 4π :

 $D(\theta, \varphi) = 4\pi \cdot \frac{power \ radiated \ per \ unit \ solid \ angle}{total \ radiated \ power}$

Gain: Accordingly the gain is defined quite similar but related to the input or accepted power of the antenna. In case of a loss free antenna (no conductional or dielectric losses) the gain is equal to the directivity.

 $G(\theta, \varphi) = 4\pi \cdot \frac{power \ radiated \ per \ unit \ solid \ angle}{input \ (accepted) \ power}$

Radiation efficiency: The antenna radiation efficiency is defined as the ratio of gain to directivity or equally the ratio between the radiated to accepted (input) power of the antenna:

$$G(\theta, \varphi) = e_{rad} \cdot D(\theta, \varphi)_{or} P_{rad} = e_{rad} \cdot P_{in}$$

Total efficiency: The total efficiency is defined as the ratio of radiated to stimulated power of the antenna:

$$P_{rad} = e_{total} \cdot P_{stin}$$

Compared to the input power the stimulated power consider any occurring reflections at the feeding location.

Reflection efficiency: The reflection efficiency is defined as the ratio of input to stimulated power. In CST MICROWAVE STUDIO® this value can also be determined from the reflection factor:

$$e_{refl} = \frac{P_{in}}{P_{stim}} = \frac{e_{total}}{e_{rad}} = 1 - S_{11}^2$$



Tips & Tricks to obtain accurate farfield results



Tip 1/3 : Check Energy



 The accuracy level in the T-solver should be -40dB.
 For larger frequency bands (eg 0-3 GHz) or bad radiation better use -60dB, so that E+H on the bounding box do not suffer from FFT/DFT truncation error.



Tip 2/3 : Check ,add. space'



"open (add space)" boundary ensures $\lambda/8$ space at the center frequency, for lower frequencies (bigger λ) the space needs to be increased accordingly.



Tip 3/3 : Check Balance



Farfield values become critical, *if S-Parameter balance=1* (no power is radiated). In this case directivity and gain are calculated from dividing 0/0, which is numerically critical.
 A good measure for total radiated power is: (1-balance).



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How to calculate farfield Broadband at many frequencies



Definition of Broadband Farfield Monitors

Solve Results Macros Window Help Farfield Broadband Farfield Monitors File × Calculate monostatic RCS Filter Analysis ٠ **Farfield Slant Polarization** ۲ GRASP feed file export Graphics E G Field Monitors -🗘 ff 01.0000 - c ff_01.5000 - c ff_02.0000 - c ff_02.5000 Definition of Farfield Monitors X - C ff_03.0000 - C ff_03.5000 frg low 1 -ct> ff_04.0000 -ct ff 04,5000 fra high 10 -🗘 ff 05.0000 -🗘 ff 05.5000 frg stepsize 0.5 -🗘 ff 06.0000 -🗘 ff 06.5000 Cancel Help -🗘 ff 07.0000 0K -🗘 ff 07.5000 -c ff 08.0000 -c ff 08.5000 -c ff 09.0000 -c ff 09.5000 🗘 ff 10.0000



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 macro can be applied *multiple times* without overwriting the previous definitions, so that different frequency resolutions can be combined.

Evaluation of Broadband Farfield Monitors



Definition of Farfield Probes

Farfield *monitors* record the radiation in ALL directions for ONE frequency.

Farfield *probes* record the radiation in ONE direction for ALL frequencies. (recording a time signal)



90

40





Phi

Radius

Results from Farfield Probes





Optimizing Farfield Results



Optimizing Farfield Results

Template Based Postprocessin	e 🔰	3
1D Results OD Results		
+ 0D Value from 1D Result + 0D Value from 2D 3D Plot + Mix 0D Results 3D Eigenmode CoupleCoefficient 3D Eigenmode Result Evaluate Field in arbitrary Coordina Evaluate Field on predefined Curve Evaluate Field on predefined Face Farfield Get Number of Meshcells Phased Array Result Port Impedance S Parameter	tes (OD, 1D, 2D, 3D)	
Settings Delete Duplic	Farfield Monitor and Excitation ff_04.6000 ✓ [1] Plot Range Result Value Polar Plot ✓ Max. Value Cutplane Max. Value ✓ Varying Angle Theta Phi Stepsize: 5 deg	Plot Mode and Scaling Gain (IEEE) Component: Abs Pol.Vector (x/y/z): 0 Pol.Vector (x/y/z): 0 Reference Distance: 1 O linear O log (dB) Nearfield dB Units: dBV/m, dBA/m, dBW/m2
	OK Cancel Help	Phase Center Options



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15

Example: 3dB Angular Width



Define Goal from 0D Template



all existing 0D Result Templates can be used to define goals for optimization runs.



Co & Cross Polarization



Co & Cross Polarization



The **Co-polarized** farfield component has the same polarization as the excitation (y-oriented in our case).

The **Cross-polarized** farfield component is orthogonal to Co-pol component and mainlobe direction.

In order to use different polarizations for transmitting/receiving, an antenna design goal might be to maximize the Co-pol and minimize the cross-pol component.



Co & Cross Polarization Adjust the Axes / coord. system



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worse for the angles phi=45 and phi=225

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Co & Cross Polarization Result Templ. for Param-Sweep & Optimization

🗟 1D Farfield Plot Co pol = Ludwig 3 Vertical Farfield Monitor and Excitation Plot Mode and Scaling 20 v Gain (IEEE) farfield (f=5) 10 [1] Component: Ludwig 3 Vertical Excitation String: Û. V -10 Pol.Vector (x/y/z): 0 0 Cutplane -20 Varying Angle Fixed Angle Reference Distance: -30 Theta: 💿 Theta 🛛 🔿 Phi 🔘 linear 💿 log (dB) Nearfield -180 -100Ω 100 180 5 0 Stepsize: deg Phi: dBV/m , dBA/m, dBW/m2 🔽 Theta / Degree OK. Cancel Help 🗟 1D Farfield Plot × Cross pol = Ludwig 3 Horizontal -10 Farfield Monitor and Excitation Plot Mode and Scaling -15 Gain (IEEE) farfield (f=5) -20 [1] Ludwig 3 Horizontal Excitation String: Component: -25 0 Pol.Vector (x/y/z): Cutplane -30 **Fixed Angle** Varying Angle Reference Distance: -180 -100100 180 Ω Theta: 💿 Theta 🛛 O Phi 💿 log (dB) Nearfield Inear Stepsize: 5 45 deg Phi: dB Units: dBV/m, dBA/m, dBW/m2 💉 Theta / Degree CST 0K Cancel Help www.cst.com

Phase Center / Grasp Export



Phase Center Calculation

Farfield Plot General Plot Mode Axes Origin Array Decoupling Plane Phase Center	Finding the best location to place the horn inside a dish antenna. The best position is to match the <i>focal point of the dish</i> with the <i>phase center of the horn</i> .
Calculate phase center E-Field component Theta Phi Angular limit around z'-axis Angle: 15 deg.	
Type = Farfield Approximation = enabled (kR >> 1) Monitor = farfield (f=5) [1] Component = Ludwig 3 Ver. Phase Output = E-Field(r=1m) Frequency = 5 Emox(Thoto) = 20 41 JPU/m Phase center = (2, 1, 5,29659) Sigm	a A-0829187 (H-Plane)
rnase center = (2, 1, 5.23653) 519m	a 0.0023107 (N-FIANE)



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Check Phase Center by plotting Ludwig3-Ver.Phase

Plotting the Phase of Ludwig 3 Vertical (=dominant component co-pol) does not result in a phase 180 deg jump (=colour jump) at theta=0



Check Phase Center by moving Origin into Phase Center



Farfield Data Export in Grasp Format



Circular Polarized Antennas



Circular Polarized Antennas



 Transient Solver Parameters

 Solver settings

 Accuracy:

 -50

 -50

 Stimulation settings

 Source type:

 All





only mode 1 active



only mode 2 active





Combining the Results

Monitor combination







view in -z direction



Combining the Results

Monitor	combina	ation	Automatic labelin	g
Label:	circ			
List:				•
Port mod	de	Amplitude	 Phase shift	~
1 (1)		1	0	
1 (2)		1	90	



Ports=ALL/Modes=All + Combine Results

- requires several T-runs (-> use Distributed Computing!)
- + produces S-Parameters
- + broadband constant phase shift of 90 deg.
- + flexibility to get results for arbitrary am/ph combination in postproocessing

Simultaneous Excitation

- + only one run required
- produces F-Parameters (no S-Parameters)
- constant phase shift only valid for one frequency
- different am/ph combination requires new run





Farfield Capabilities for circular polarized Antennas



Result Template for Combined Monitor 1[1.0,0.0]+2[1.0,90],[80]

Farfield 'farfield (f=60) [1[1.0,0.0]+2[1.0,90],[80]]' Gain_Abs(Theta)

Solver settings Source type: 30 to be set manually !! Studiences Source type: Getected Port T Calculate mo Source type: Getected Port T Source type: Getected Port	Solver Parameters		2	×I 90		-	
Simulation settings Source type: Selected Plots Full deembed Fort mode Each Attion Selection Source type: Selected Plots Full deembed Fort mode Each Attion Selection Fort Mode Angle Fort	Solver settings Accuracy: -30 💌 d	B 🔲 Store result data	a in cache Ootimine		60	Note: In a the	all farfield result templates Excitation string has
Source type: Selected Ports Full deended Port mode latt Calculate mo Separameter setting: Nominate to fixed impedance Sparameter Separameter setting: Nominate to fixed impedance Sparameter Sparameter setting: Network computing Network (computing Network computing Network computing Netwo	Stimulation settings	P	Port Mode Excitation Select	tion	×.	to	he act manually II
Pottmode let: Calculate mo Sparaneter setting: Calculate mo Nominice to find inpodence Sparameter setting: Adaptive mesh refinement Adaptive mesh refinement Adaptive mesh refinement Adaptive mesh refinement Network computing Vetwork proces Vetwork proces Simulaneous exclusion Vetwork proces Vetwork proces Vetwork proces Simulaneous exclusion Vetwork proces Vetwork proces Vetwork proces Vetwork proces Vetwor	Source type: Selected Ports	🔲 Full deembed	Port mode Amp	pli. Phase shift Signal	Set all		
Sparameter settings Normalize to fixed impedance Sparameter Adaptive mesh refinement Adaptive mesh refinement Network computing Network comp	Port mode list	Calculate more	x 1 1.0	90 default	Set none	It IS I	ecommended to use
Spatialities during Spatialities (study) instead of the automatic number- labelling. Adaptive mesh refinement Adaptive mesh refinement Adaptive mesh refinement Network computing Network computing Network computing Network computing Network computing Network c	- S parameter politings					a snort	er userdefined labelling
Image: Specemeter Adaptive mesh refinement: Frequency: = 60 Main lobe magnitude = 155.d B Main lobe magnitude = 15.5.d B Main lobe magnitude = 15.5.d B Main lobe level = -5.0.dB 30	Normalize to fixed impedance	🔲 S-parameter :				inst	ead of the automatic
Adaptive mesh refinement Adaptive mesh refinement Network computing Network proce Simultaneous excitation Network proce Network proce Network proce Network proce Simultaneous excitation Network proce Simultaneous excitation Network proce Network proce	50 Ohms	S-parameter			Γοκ	r	number- labelling.
Adeptive mesh refinement. Adeptive proce Network computing Simultaneous excitation ✓ Activate Activate Label: Itilicity Lit: Circuity 150 Time delay Frequency = 60 Main lobe direction = 5.0 deg. Angular width (3 dB) = 12.2 deg. Side lobe level = -5.0 dB 120	Adaptive mesh refinement				Consel 1		1
Network computing Simultaneous excitation Network computing Network prope Image: Simultaneous excitation Image: Simultaneous excitation Image: Side lobe level = -5.0 dB Image: Simultaneous excitation Image: Side lobe level = -5.0 dB Image: Simultaneous excitation Image: Side lobe level = -5.0 dB Image: Simultaneous excitation Image: Side lobe level = -5.0 dB Image: Simultaneous excitation Image: Side lobe level = -5.0 dB Image: Simultaneous excitation Image: Side lobe level = -5.0 dB Image: Simultaneous excitation	Adaptive mesh refinement	Adaptive prope		😤 Farfield OD I	Result		×
Network computing Network proce Image: Computing I	Network computing		_ Simultaneous excitation	Farfield Moni	itor and Excitation	¥	Plot Mode and Scaling
Image: Include the incl	Network computing	Network prope	Activate	farfield (f=60) -	+2[1.0,90],[80]	Gain (IEEE)
List ,, CirC" 15d , Circ" Nain lobe magnitude = 15.5 dB , Circ" Main lobe direction = 5.0 deg. , 120 120 , Circ" 0K Cancel Side lobe level = -5.0 dB 90			Label: 1[1.0,0.0]+2[1.0,90]		Devilt		
Frequency = 60 Main lobe magnitude = 15.5 dB Main lobe direction = 5.0 deg. Angular width (3 dB) = 12.2 deg. Side lobe level = -5.0 dB			List:	Plot Range-		"CirC"	Component: Abs
150 Time delay Phase shift 150 Time delay Phase shift Varying Angle Fixed Angle Theta 90		N	"CITC"		Max. V	alue	Pol.Vector (x/y/z): 0 1 0
Frequency = 60 Main lobe magnitude = 15.5 dB Main lobe direction = 5.0 deg. Angular width (3 dB) = 12.2 deg. Side lobe level = -5.0 dB		150	C Time delay 💿 Phase s	shift Cutplane —	ala — Fiva	d Angle	Reference Distance: 1 m
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Angular width (3 dB) = 12.2 deg. 120 OK Cancel Side lobe level = -5.0 dB 90	Main lobe di	irection = 5.0 de	 .g.	-			
Side lobe level = -5.0 dB	Angular widt	th (3 dB) = 12.2 de	- 120 - eg.	ОК	Cancel		
	Side lobe le	vel = -5.0 dB		90			



Summary

- Antenna Farfield can be recorded in time and frequency domain (Probe / Monitor)
- Postprocessing templates automize result extraction (e.g. broadband farfield)
- checklist for accurate farfield:
 - energy decayed to -40dB [-60dB] ?
 - enough surrounding space ($\lambda/8$) open (add space)?
 - Is antenna radiating at this frequency? (S-balance<1?)
- Advanced capabilities to extract: co+cross-pol / phase center / Grasp input data RL pol / axial ratio

